## **PIP-II Beam Transfer Line Quadrupoles**

V. Kashikhin, July 11, 2018

0.1%, and maximum current 13 A. magnet aperture 52 mm, good field region 24 mm, field non-linearity in the good field region There needed 49 quadrupoles with the effective length of 0.2 m, integrated gradient 2 T, the

magnet parameters presented in Table 1. There were investigated number of variants including indirect and direct water cooling. These easiest to tabricat

Magnet power Number coolin Cooling hole di Water pressur Water temper Number magn	Magnet Numbe Cooling Water I Water 1	Magnet Numbe Cooling Water I	Magnet Numbe Cooling	Magnet Numbe Cooling	Magnet Numbe	Magnet	INIGRIE	- 24,220	Windin	Yoke length	Coil nur	Coil cop	Coil pea	Coil am	Pole tip field	Center:	Integrat	Pole tip radius		Name	
Voltage for the string		Number magnets in string	Water temperature rise	Water pressure drop	Cooling hole diameter	Number cooling circuits	power	Magnet voltage	Winding resistance	ngth	Coil number of turns	Coil copper conductor	Coil peak current	Coil ampere-turns/pole	field	Center field gradient	Integrated gradient	radius			
<	:		С	MPa	mm		8	٧	Ohm	mm		mm	A	Α	Т	T/m	Т	mm		Units	
228	3	14	2.2	0.1	5	1	212	16.3	1.25	200	210	2.6x2.6 (AWG10)	13	2800	0.26	10	2	26	cooling, 13A	Indirect water	
02	( A2	14	6.2	0.1	5	1	221	4.42	0.088	200	54	7x7, dia. 5	50	2800	0.26	10	2	26	cooling, 50A	Direct water	
40	62 E	14	8.8	0.1	5	1	446	4.46	0.045	200	28	7x7, dia(5)	100	2800	0.26	10	2	26	cooling, 100A	Direct water	

## 14 magnets

iron yoke is not saturated. Fig. 2 shows longitudinal field distribution at the reference radius of 12 mm for 0, 30 deg., 45 deg. angles. Results of preliminary 3D magnetic field analysis shown in Fig. 1 - Fig. 2. Fig. 1 shows that the

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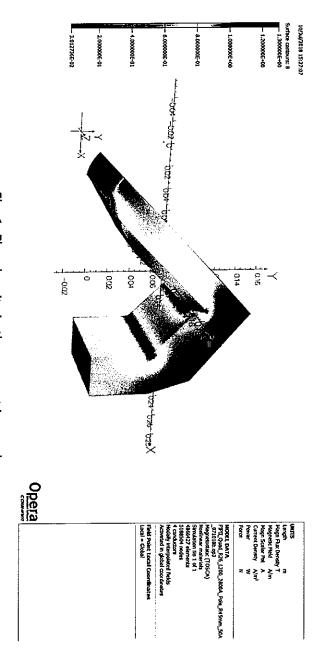


Fig. 1. Flux density in the magnet iron yoke.

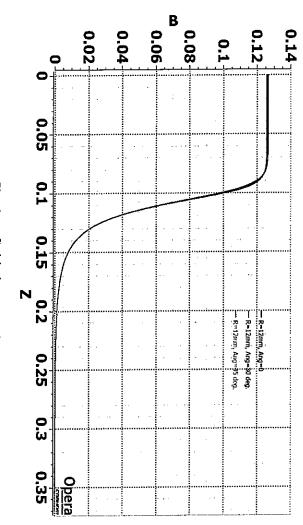


Fig. 2. B-field along Z-axis.

reference radius 12 mm. The integrated field non-linearity for this variant is less than the specified 0.1 % value for the

Fig. 3 – Fig. 5 shows the preliminary magnet cross-sections for all three variants.

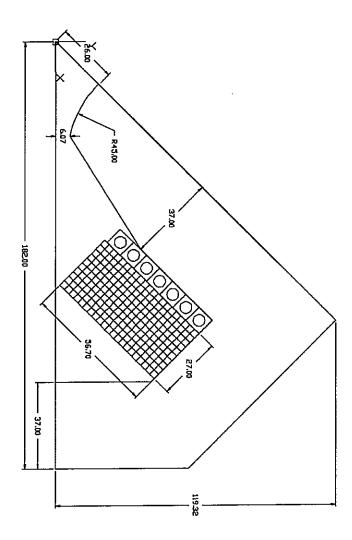


Fig. 3. Quadrupole with indirect water cooling and current 13 A.

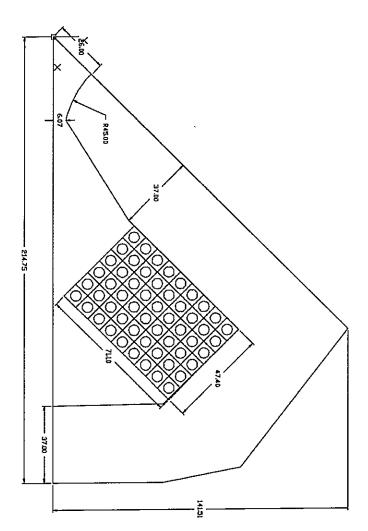


Fig. 4. Quadrupole with direct water cooling and current 50 A.

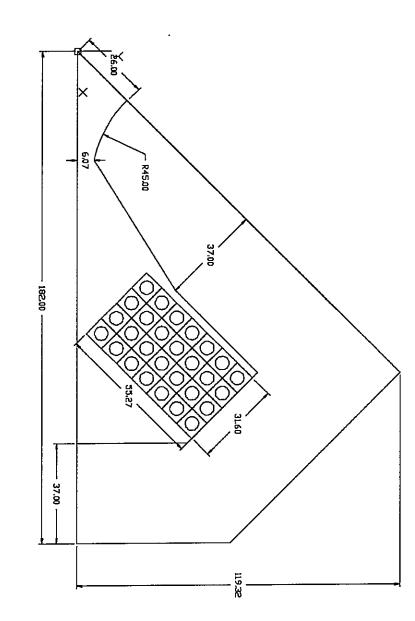


Fig. 5. Quadrupole with direct water cooling and current 100 A.

## Summary

there are 6 end of line quadrupoles with 3 T integrated gradients which will need even more voltage. Because string of magnets is connected in series, the cabling is not an issue. Besides cooling. The cost of power supply is proportional to the power, and not depend on current and cooling design is more straightforward for the fabrication, and provides more reliable, stable same length. Even more compact water cooled magnets with lower current could be designed if But these magnets will need 50% more current to obtain 50% larger integrated gradient at the direct water cooling magnets, because there is some margin in the iron flux density, and cooling. cooling capacity. The preliminary analysis showed that these quadrupoles could be identical to reduce the conductor cooling hole diameter from 5 mm to 4 mm. It is possible to design and fabricate any of these three magnet variants. But the direct water